



(1) Publication number: 0 493 302 A1

12

EUROPEAN PATENT APPLICATION

(21) Application number: 91630104.7

(22) Date of filing: 05.12.91

(51) Int. Cl.⁵: **F16L 43/00,** F15D 1/04

30 Priority: 24.12.90 US 632685

(43) Date of publication of application : 01.07.92 Bulletin 92/27

84 Designated Contracting States : DE ES FR GB IT

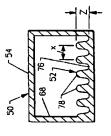
71 Applicant: UNITED TECHNOLOGIES CORPORATION
United Technologies Building 1, Financial Plaza
Hartford, CT 06101 (US)

(72) Inventor: Presz, Walter M., Jr.
 40 Grove Street
 Wilbraham, Massachusetts 01095 (US)

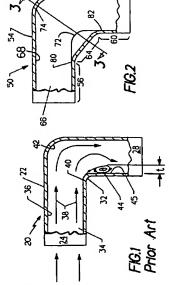
(4) Representative: Weydert, Robert et al Dennemeyer & Associates Sarl P.O. Box 1502 L-1015 Luxembourg (LU)

(54) Mechanism to reduce pressure losses in angled conduits.

Downstream extending convolutions (52) disposed on the inside corner (72) of an angled conduit (50) eliminate or reduce the two-dimensional boundary layer separation region (44) thereby eliminating or reducing the pressure losses associated with the separation region (44) in prior art angled conduits. The convolutions (52) may be formed into either the angled conduit wall or in an insert which is positioned on the inside comer surface of the conduit.







15

25

30

35

40

45

Technical Field

This invention relates to flow in conduits.

Background Art

A major problem with flowing a fluid through a conduit, such as a duct or pipe, is the pressure losses which accumulate over the distance travelled by the fluid. A principal source of the losses is two-dimensional boundary layer separation which occurs immediately downstream of sharp turns in the conduit.

Separation is a result of the lack of momentum in the boundary layer of the flow in the new direction dictated by the turn in the conduit. This causes the boundary layer along the surface of the inside corner of the conduit to detach from the surface immediately downstream of the turn. The fluid adjacent to the conduit surface in the separation region flows in the reverse direction, due to the inability of the momentum of the flow to overcome the back pressure in the flow, and interaction with the flow of the bulk fluid produces an eddy which recirculates the fluid. The recirculation removes energy from the flow and results in a pressure loss proportional to the size of the separation region.

Another problem associated with the separation region is the pressure pulses generated in the flow as the re-attachment point of the bulk fluid fluctuates in position. The re-attachment position is the downstream point where the separation region ends and the flow of the bulk fluid contacts the surface again. The position of the re-attachment point fluctuates as the size of the separation region varies and larger separation regions produce larger pressure pulses. The generation of the pressure pulses increase the instability of the flow and can damage, or increase the noise level associated with, components actuated by the flow

One method to overcome the loss in fluid pressure is to increase the pressure of the fluid at the inlet of the conduit by an amount equal to the accumulated pressure losses. This solution is undesirable due to the added cost of producing a higher inlet pressure and of fabricating a conduit around the increased pressure requirements. Additionally, this solution would generate larger separation regions and larger pressure pulses. Another solution is to route the flow such that turns are kept to a minimum. Although a conduit without any turns would be ideal, for many purposes a straight conduit is impractical. It is, therefore, highly desirable to conduct a flow of fluid through an angled conduit with minimal pressure losses.

Disclosure of Invention

An object of the invention is to eliminate or decrease the extent of the separation region on the inside

corner wall of a bend in a conduit and to thereby reduce pressure losses in the flow.

Another object is to eliminate or reduce pressure pulses in the flow.

According to the present invention, a convoluted surface on the inside corner of conduit bend provides a means to reduce or eliminate the separation region associated with flow around the corner. The convoluted surface, which is configured to generate large scale vortices, produces a flow variation which disrupts the eddy flow in the separation region, thereby reducing turning losses. The size and shape of the convolutions are selected to delay separations of the fluid from the surface of the convolutions, preferably around the entire corner, but certainly further downstream as would otherwise occur.

"Large scale" vortices as used herein means vortices with dimensional characteristics of the same order of magnitude as the maximum height of the convolutions.

More particularly, a conduit for a fluid flow has a bend or comer portion, with a convoluted surface located at the inner comer of the corner portion. The convoluted surface consists of a plurality of downstream extending, adjoining, alternating troughs and ridges which preferably blend smoothly with each other along their length to form a smooth undulating surface.

It is believed that the troughs and ridges eliminate or reduce the extent of the separation region downstream of the corner by producing a flow variation which disrupts the eddy flow in the separation region and allows the boundary layer to re-attach sooner. and by delaying separation as the fluid flows around the corner. The flow variation is the result of the lateral momentum picked up by the fluid which flows through the troughs and which generates a spiralling motion in the fluid. It is this spiralling motion about an axis normal to the axis of the eddy flow which disrupts the recirculation in the separation region. By reducing the size of the separation region the pressure losses associated with the flow travelling around a corner are reduced. In addition, the reduction in size of the separation region improves the stability of the flow and reduces the magnitude of the pressure pulses generated by the separation region.

The foregoing and other objects, features and advantages of the present invention will become more apparent in the light of the following detailed description of preferred embodiments thereof as illustrated in the accompanying drawings.

Brief Description of the Drawings

FIG. 1 is side view of a flow conduit having a corner in accordance with prior art.

FIG. 2 is a side view of a flow conduit of rectangular cross-section with a convoluted surface on the

15

20

25

30

35

40

4

inner comer surface in accordance with the present invention.

FIG. 3 is a sectional view taken along line 3-3 of FIG. 2.

FIG. 4 is a side view of a flow conduit of circular cross-section with a convoluted surface on the inner corner surface.

FIG. 5 is a sectional view taken along line 5-5 of FIG. 4.

FIG. 6 is an illustration of the vortices generated by flow over a convoluted surface.

FIG. 7 is an illustration of the vortices generated by the convoluted surface.

FIG. 8 is a side view of a flow conduit with a convoluted flow insert.

FIG. 9 is a perspective view of the convoluted flow insert of FIG. 8.

FIG. 10 is a sectional view taken along line 10-10 of FIG. 8.

FIG. 11 is a graph of pressure rise coefficient as a function of downstream position for a conduit with and without a convoluted surface on the inside corner of the inner wall.

Best Mode for Carrying Out the Invention

Referring now to FIG. 1, a conduit 20 in accordance with prior art comprises a wall 22 defining an upstream conduit portion 24, a downstream conduit portion 28, and a corner portion 32 joining the upstream conduit portion 24 and downstream conduit portion 28. The internal surface 36 of the wall 22 defines a fluid passage 34 with the fluid flow direction indicated by arrows 38. The internal surface 36 includes an inner corner surface 40 and an outer corner surface 42.

The change in direction of the flow within the corner portion generates a two-dimensional boundary layer separation region 44 which extends to a reattachment point 45 located on the surface 36. Separation occurs when the momentum in the boundary layer along the inner corner surface 40 cannot overcome the back pressure as the fluid travels downstream. At this point the flow velocity reverses direction, relative to the velocity of the adjacent bulk fluid, and the boundary layer breaks loose, or separates, from the inner corner surface 40. Separation results in a recirculation of the fluid about an axis perpendicular to the downstream direction of the flow. The recirculation removes energy from the fluid flow and produces pressure losses in the flow proportional to the size of the separation region 44.

Referring now to FIGS. 2 and 3, a rectangular conduit 50 similar to the conduit 20 of FIG. 1 is shown, but it incorporates the teaching of the present invention. The conduit comprises a wall 54 defining an upstream conduit portion 56, a downstream conduit portion 60, and a corner portion 64 joining the

upstream conduit portion 56 and downstream conduit portion 60. The internal surface 68 of the wall 54 defines a fluid passage 66. The internal surface includes an inner corner surface 72, an outer corner surface 74. In accordance with the present invention, the inner corner surface 72 includes of convolutions 52 (Fig. 3).

The convolutions 52 are a series of downstream extending, alternating, adjoining troughs 76 and ridges 78. The troughs 76 and ridges 78, in this exemplary embodiment, are basically U-shaped in cross-section, as shown in FIG. 3, and blend smoothly along their length to form the undulating corner surface 72 extending from the entrance to the exit of the corner. In this embodiment the height of the ridges 78 increases gradually from the upstream end 80 to a maximum and then decreases gradually to zero at the downstream end 82.

A circular conduit 100 which incorporates the troughs 102 and ridges 104 (ie: convolutions) of the present invention is shown in FIGS. 4 and 5. The ridges 104 gradually increase in height from the upstream end 103 to a maximum and then decrease to zero at the downstream end 105. One difference between this embodiment and the embodiment of FIGS. 2 and 3 is the decreasing height of the ridges 104 from a maximum at the central flow plane 108 to a minimum at the sides 110,112 of the conduit 100. This difference takes into account the curvature of the inner surface 114 as well as the expected reduced separation region thickness as one moves away from the central flow plane 108 toward the left and right sides 110,112 of the conduit 100.

The troughs and ridges are believed to reduce or eliminate the separation region by producing a flow variation which disrupts the eddy current and allows the boundary layer to re-attach to the inside wall further upstream than would otherwise occur. As shown in FIG. 6, fluid flowing through the troughs 120 and over the ridges 124 acquires lateral momentum as it exits the troughs due to the low pressure region existing immediately downstream of the ridge 124. The result is the generation of adjacent pairs of counterrotating vortices 126, initially about an axis 128 parallel to the bottom surface of the troughs.

As shown in this illustration, the ridges 124 increase in height to essentially their downstream end and then decrease in height rather abruptly.

As shown in FIG. 7, the spiralling flow, aided by the movement of the bulk fluid flow, is directed into the region where separation would normally occur, thereby disrupting the build-up of a large scale eddy.

Reducing the size of the separation region reduces the pressure losses associated with the turn in a conduit. The reduction in size of the separation region also improves the stability of the flow and reduces the magnitude of pressure pulses generated.

To have the desired effect of eliminating or signifi-

55

15

20

25

30

cantly reducing the extent of the separation region, it is believed that certain parametric relationships should be met. These parametric relationships are based on empirical data, known flow theory, and hypothesis concerning the phenomenon involved. First, the maximum height of the ridges (peak to peak wave amplitude Z, see FIG. 3) should be of the same order of magnitude as the thickness ("t" in Fig. 1) of the separation region expected to occur immediately downstream of the inner corner if the convolutions were not present.

Second, it is believed that the angle Ø between the bottom surface of the troughs (which is here shown as being straight over a substantial portion of the corner) and the direction of flow upstream of the corner (see FIG. 7) is best between 20 degrees and 45 degrees, with approximately 30 degrees being preferable. If the angle Ø is too small, the vorticity generated is insufficient. If the angle Ø is too large, flow separation will occur in the troughs.

Third, it is believed that the aspect ratio, which is defined as the ratio of the distance between adjacent ridges (wavelength X, see FIG. 3) to the wave amplitude or ridge height Z, is preferably no greater than 4.0 and no less than 0.2.

Finally, it is believed to be desirable to have as large a portion of the opposed sidewalls of each trough parallel to each other or closely parallel to each other in the direction in which the wave amplitude Z is measured.

A further discussion on the preferred size and shape of troughs and ridges useful in the application of the present invention is found in commonly owned U.S. Patent No. 4,789,117, which is incorporated herein by reference.

As shown in FIGs. 8 to 10, troughs and ridges may be incorporated into the inside corners of turns in conduits by means of a convoluted insert. The convoluted insert 200 is comprised of a base 204 which is shaped to conform to the inner corner 206 of the conduit 202. The base 204 includes a plurality of alternating ridges 208 and troughs 210, similar to the ridges and troughs of previous embodiments. The same trough and ridge parametric relationships which were discussed previously for the embodiments shown in FIG. 2 to 4 are applicable to the embodiment of FIGS. 8 to 10, except the bottoms of the troughs have a continuous curvature and the angle Ø is therefore variable.

Tests were performed to evaluate the effectiveness of a convoluted surface in reducing pressure losses in the corners of conduits. The tests were performed using air as the fluid and a test rig which consisted of a duct of rectangular cross-section (width=21.25 inches, height=5.4 inches), and either a right angle turn without convolutions on the inside corner (similar to FIG. 1) or a right angle turn with convolutions on the inside corner (similar to that shown in

FIGs. 2 and 3). The convolutions had a maximum height Z of 0.75 inches and a wavelength X of 1.10 inches, which results in a height to wavelength ratio of 0.68. Apparatus was tested wherein the angle Ø between the bottom surface of the troughs and the flow direction upstream of the comer was at 20 degrees, 30 degrees, and 45 degrees, respectively. Upstream static wall pressure and the fluid flow dynamic pressure were measured at a point sufficiently far upstream of the corner to eliminate the possibility of any effects of the turn on these measurements. Static wall pressure was also measured at several points downstream of the turn in order to be able to determine pressure loss, due to a turn, as a function of downstream position. In addition, measurements of downstream static wall pressure were taken along the inner wall and the outer wall (inner and outer relative to the radius of the turn).

The results of the test with \emptyset = 30 degrees are shown graphically in FIG. 8, which is a plot of pressure rise coefficient (Cpr) as a function of downstream location for points on both the inner corner and outer corner wall. The curves A_1 and A_2 are for a conduit without the convolutions of the present invention. A₁ represents outer corner wall points and A2 represents inner corner wall points. B1 and B2 are for a conduit with convolutions on the inner corner. B1 represents points on the outer corner wall and B2 represents points on the inner corner wall. Cpr is calculated by subtracting the downstream wall pressure at a particular point from the upstream wall pressure and dividing by the dynamic pressure. Larger pressure losses, therefore, produce larger values of Cpr. The results confirm that the corner with convolutions produced lower pressure losses than the corner without convolutions and, for the embodiment used in this test, there was a 15% to 20% decrease in pressure loss.

The embodiments illustrated in FIGS. 2 through 10 shows the invention used in conduits with right angle turns. The invention should reduce pressure losses in conduits with turns of any angle which produce two-dimensional boundary layer separation. In addition, even though the embodiments illustrated were incorporated in conduits with rectangular and circular cross-sections, the invention is equally applicable to conduits of other cross-sectional shapes.

Although the invention has been shown and described with respect to exemplary embodiments thereof, it should be understood by those skilled in the art that various changes, omissions and additions may be made therein and thereto, without departing from the spirit and the scope of the invention.

10

15

20

25

30

35

45

50

Claims

- 1. A conduit for carrying a fluid in a downstream direction, said conduit having wall means defining an internal flow passage and a corner portion for turning the flow, said wall means having formed therein a plurality of downstream extending, adjoining alternating troughs and ridges located on an inner corner of said corner portion, wherein said troughs and ridges extend from an upstream end of said corner portion to a downstream end of said corner portion, increase in depth and height, respectively, from said upstream end to a maximum and decrease from said maximum to zero at said downstream end, and are configured to generate large scale vortices.
- The conduit according to claim 1, wherein said troughs and ridges are U-shaped in cross section taken perpendicular to their length and blend smoothly with each other along their length to form a smoothly undulating surface.
- 3. The conduit according to claim 1, wherein said conduit is circular in cross-section.
- The conduit according to claim 1, wherein said conduit is rectangular in cross-section.
- The conduit according to claim 1, wherein the aspect ratio of said troughs and ridges is between 0.2 and 4.0.
- 6. The conduit according to claim 1, wherein each of said troughs has a bottom surface portion extending in a straight line, wherein the angle between said bottom surface portion and the direction of flow immediately upstream of said corner portion is greater than 20 degrees and less than 45 degrees.
- The conduit according to claim 2, wherein each of said troughs have opposed sidewalls which are substantially parallel to each other.
- 8. A loss reducing insert adapted to overlie and replace the inside flow surface of a turn in a fluid flow
 conduit, said insert comprising an upstream end,
 a downstream end and a plurality of downstream
 extending, adjoining alternating troughs and
 ridges, extending from said upstream end of said
 flow insert to said downstream end of said flow
 insert, said ridges increasing in height from said
 upstream end to a maximum height downstream
 and decreasing in height from said maximum to
 zero at said downstream end, and wherein adjoining troughs and ridges are configured to generate
 large scale vortices.

- 9. The insert according to claim 8, wherein said troughs and ridges are U-shaped in cross section taken perpendicular to their length and blend smoothly with each other along their length to form a smoothly undulating surface.
- 10. The insert according to claim 8, wherein the upstream portion and the downstream portion of the insert are circular in cross-section.
- 11. The insert according to claim 8, wherein the upstream portion and the downstream portion of the insert are rectangular in cross-section.
- 12. The insert according to claim 9, wherein each of said troughs has opposed sidewalls which are parallel to each other.
 - 13. The insert according to claim 8, wherein the aspect ratio of said troughs and ridges is between 0.2 and 4.0.
 - 14. Conduit means for carrying a fluid in a downstream direction, said conduit means having a bend therein which changes the direction of flow, the bend having an inside corner surface over which fluid within said conduit means is adapted to flow as it travels around the bend, said inside corner surface comprising a plurality of adjoining, alternating troughs and ridges extending in the fluid flow direction around the bend and defining a convoluted surface.
- 15. The conduit means according to claim 14 having an inside corner wall portion, wherein said conduit means includes an insert overlying said inside corner wall portion, and wherein said convoluted surface is a surface of said insert.
- 40 16. The conduit means according to claim 15, wherein the height of said ridges is on the order of the thickness of the separation region which would have been formed if said inside corner surface were not convoluted.
 - 17. A corner insert adapted to overlie and supplant the inside corner flow surface of a bend in a fluid flow conduit, said insert comprising a plurality of alternating, adjacent troughs and ridges extending in a direction which would be the downstream flow direction when the insert is in place.
 - 18. The insert according to claim 17, wherein said troughs and ridges are configured to generate a plurality of large scale vortices downstream thereof when in use.

EP 0 493 302 A1

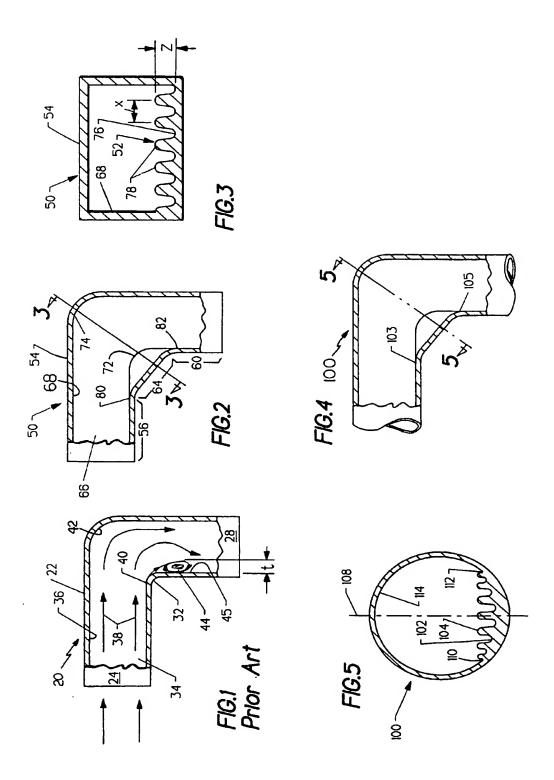
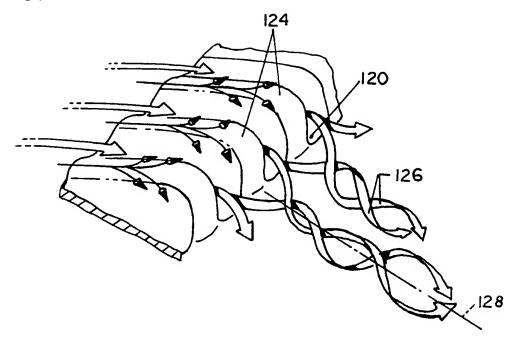
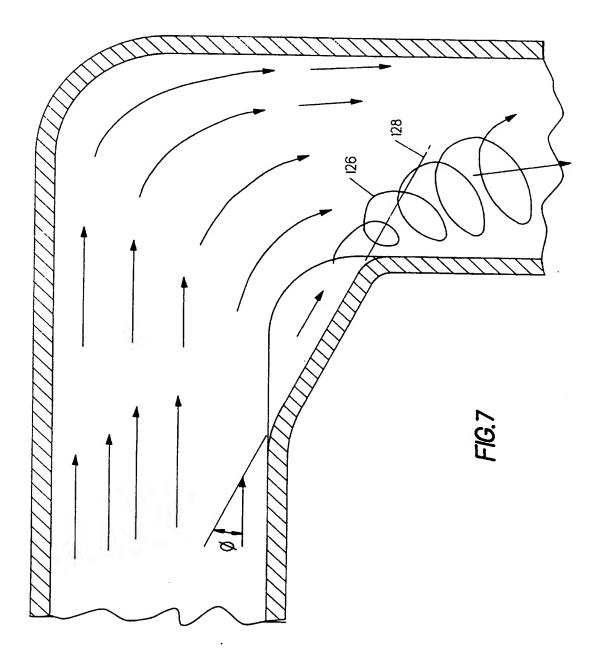
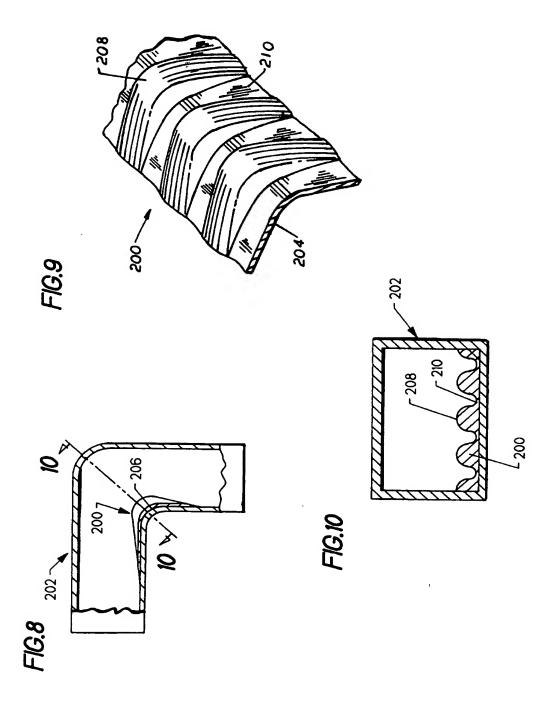


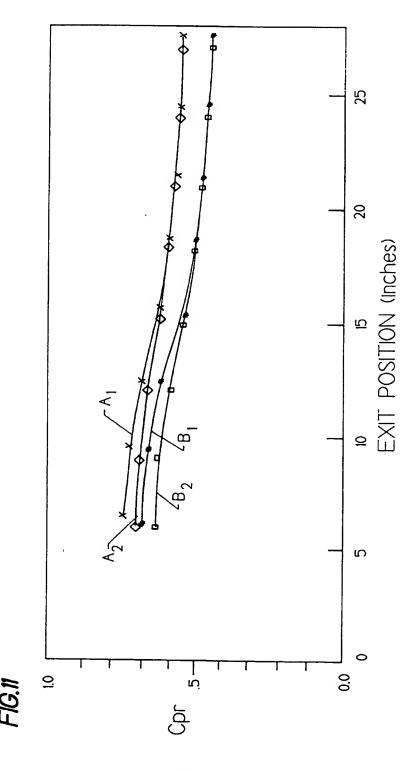
FIG.6





EP 0 493 302 A1





EP 0 493 302 A1



EUROPEAN SEARCH REPORT

Application Number

EP 91 63 0104

		IDERED TO BE RELEVAN indication, where appropriate,	Relevant	CLASSIFICATION OF TH
Category	of relevant p		to claim	CLASSIFICATION OF THE APPLICATION (Int. Cl.5.)
A	GB-A-700 615 (POWER JE	TS (RESEARCH AND	1-9.	F16L43/00 ·
	DEVELOPMENT) LTD.)		12-15,17	F1501/04
	* page 4 - page 5; fig	ures *		
A	US-A-2 705 973 (KICE)		1,2,7-9,	
			12,15,17	
	* the whole document *			
A	EP-A-0 321 379 (UNITED	TECHNOLOGIES CO.)	1-3,5,	
			7-10,	
			12-14,	
			17, 18	
	* column 1, line 26 - 4	column 1, 1tne 43; figures		
	* column 2, line 56 -	column 4, line 19 *		
	* column 9, 11ne 6 - c	olumn 9, line 44 *		
^	GB-A-1 228 223 (SIMON-	CARVES LTD.)	1,3,8,	
			10,14,17	
	* the whole document *			
				TECHNICAL FIELDS SEARCHED (Int. Cl.5)
				F16L
				F15D
	•			
			İ	
			`	
			i i	
			1	
			1	
			1	
	The masses and a second		1	
	The present search report has I	Date of completion of the search	<u> </u>	Examiner
THE HAGUE		O1 APRIL 1992	NEUM	ANN E.
	CATEGORY OF CITED DOCUME	NTS T: theory or princip	le underkrine the	Invention
		E : earlier patent do	cument, but publi	shed on, or
X: particularly relevant if taken alone Y: particularly relevant if combined with anoth-		other D: document cited i	after the filing date D: document cited in the application	
doc	ument of the same category mological background	i.: document cited f	or other reasons	***************************************
	-written disclosure	& : member of the s		***************************************